

VALID

Verification through Accelerated testing
Leading to Improved wave energy Designs



Your new platform

VALID - WEC hybrid testing: Lessons learnt from the IDOM's case study

2024-01-31

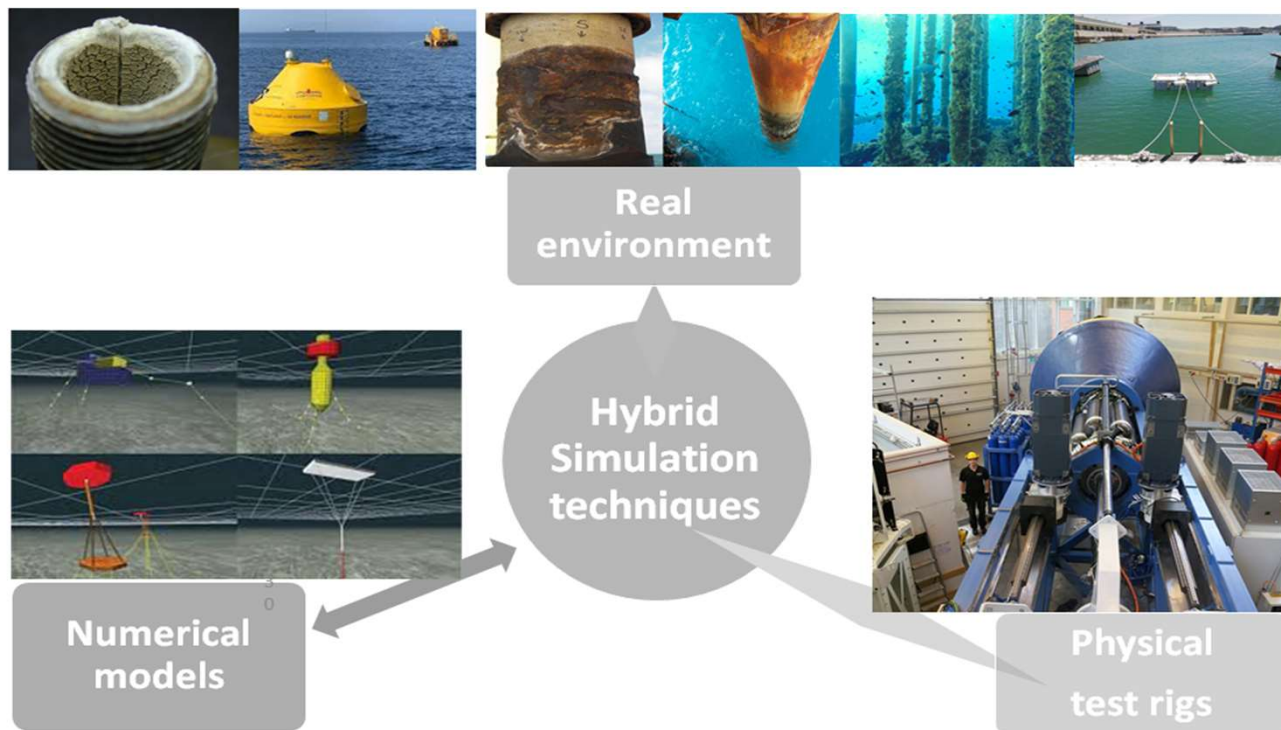
Ivan Ruibal, Eider Robles

IDOM, TECNALIA



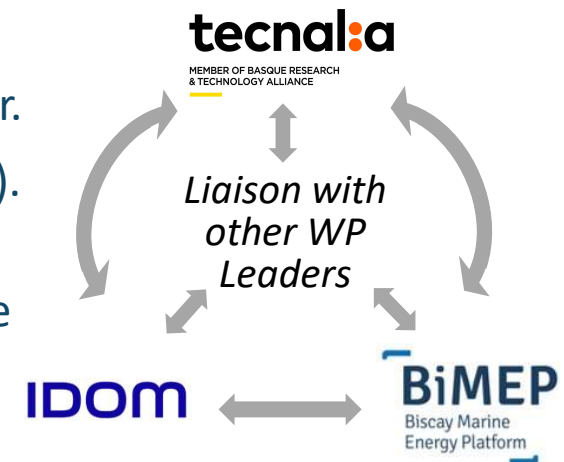
This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101006927.

What is Hybrid testing?



Electric generator failure

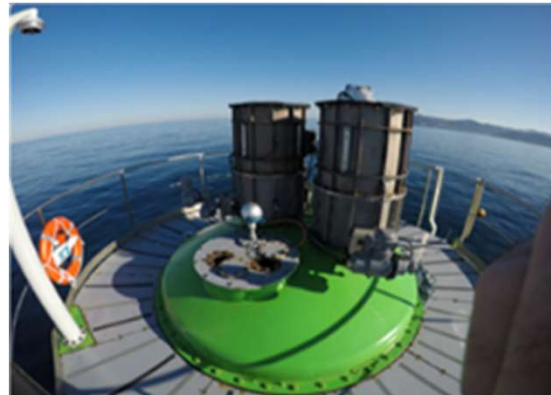
- Main aim: Produce a first-of-a-kind practical implementation of the novel testing methodology and hybrid platform on the electric generator.
- This failure mode will be exemplified on IDOM's OWC device (MARMOK).
- This technology has been extensively demonstrated at the Mutriku shoreline OWC plant (since 2011) and at the BiMEP open-sea testing site (2.5 years) within the H2020 OPERA project.



Mutriku Site



IDOM's MARMOK



TECNALIA's testbench



WHO WE ARE



Bilbao Headquarters

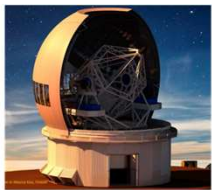
We are an independent firm providing Consulting, Engineering and Architecture professional services, united in our way of doing things, shared objectives, the Service of our clients.

4300
Professionals

65
Years of experience

920
Partners

125
Countries



Science



Transport



Energy



Environmental



Industry



Telecom



Building



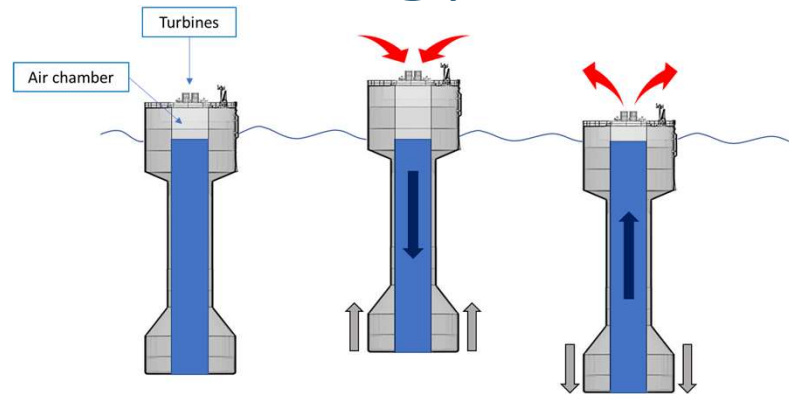
Consulting



- Advanced Design & Analysis
- Energy
- Industry
- Architecture
- Consultancy
- Transport & Infrastructures
- Water & Environment

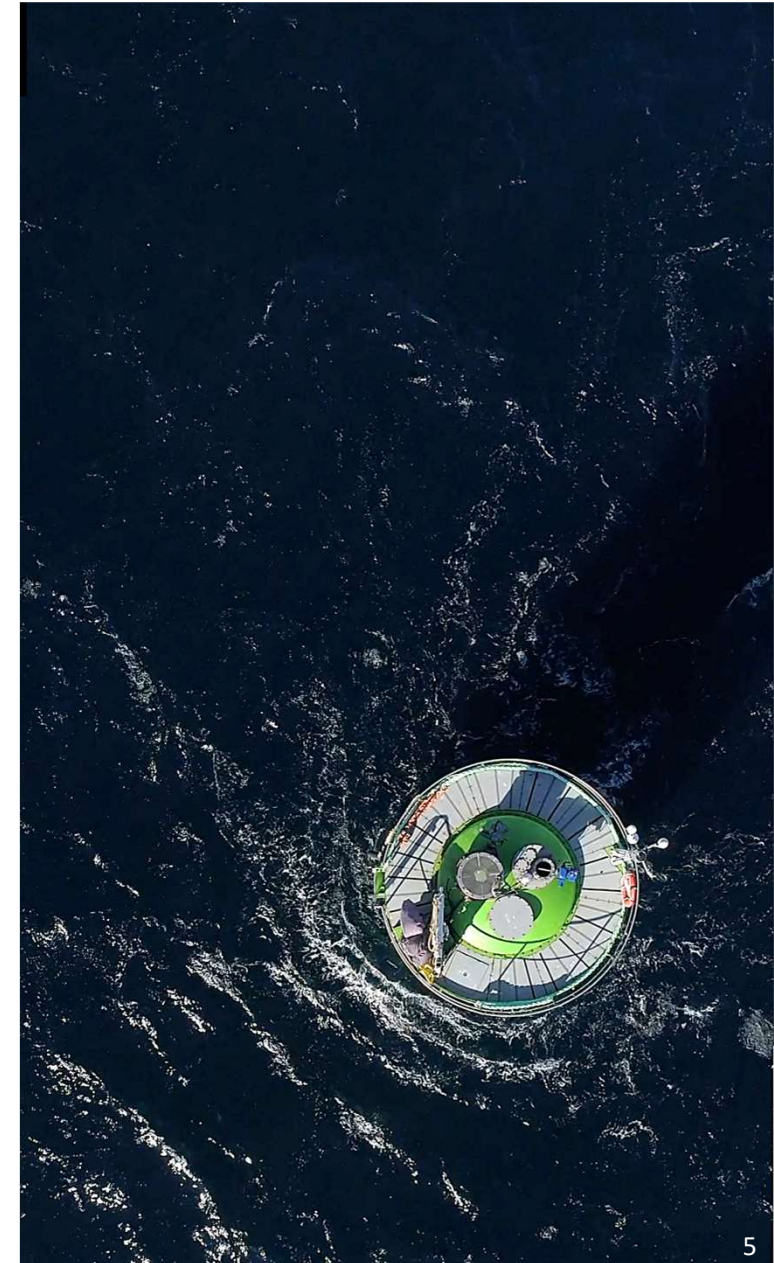
- Operating Globally
- 45 Offices Worldwide
- International activity >90%

The Technology



MARMOK's unique design provides the following advantages:

- **Simplicity:** formed by a single structural element, it avoids complex mechanisms exposed to offshore conditions. The only moving part is the turbine-generator set, which is placed on the deck and easily accessible.
- **Robustness:** 'spar buoy' configuration has been widely proved in the offshore industry to provide good performance and reliability.
- **Adaptability:** simple modifications permit the optimization of the device for a particular location and wide range of sea conditions.
- **Reduced maintenance:** due to the simplicity of the device and based on previous experience, minimum maintenance is required which supposes a substantial number of operating hours.
- **Potential to achieve a competitive LCOE**



MARMOK WEC Technology

- Activities around marine renewables started 12 years ago with the development of a wave energy harvesting technology (Spar type OWC)
- Technology with outstanding simplicity, robustness and maintainability (a single moving part, not submerged)
- Viability of the technology demonstrated offshore during 2.5+ years (3 consecutive winters)



Mutriku Wave Power Plant



The Mutriku wave plant achieves cumulative electricity production of three million kilowatts per hour

11 ENE 2024

- The Mutriku plant is the first commercial plant in Europe to use wave energy to generate electricity, the longest-lived in the world and the one with the most hours of operation.
- It has reached 12 and a half years of continuous clean energy production, with an annual production of approximately 300,000 kWh.

The wave plant of Mutriku, the first worldwide commercial project associated with the wave power sector, has surpassed a new milestone in the field of wave energy by reaching cumulative electricity production of three million kilowatts per hour.

The Mutriku plant is the first European commercial plant that uses wave energy to generate electricity, the world's oldest and the one that accumulates more hours of operation. Since its launch in 2011, the Mutriku wave energy plant has been 12 and a half years old, generating clean energy continuously. It has passed several stages of development and has exceeded the production records achieved so far by a renewable

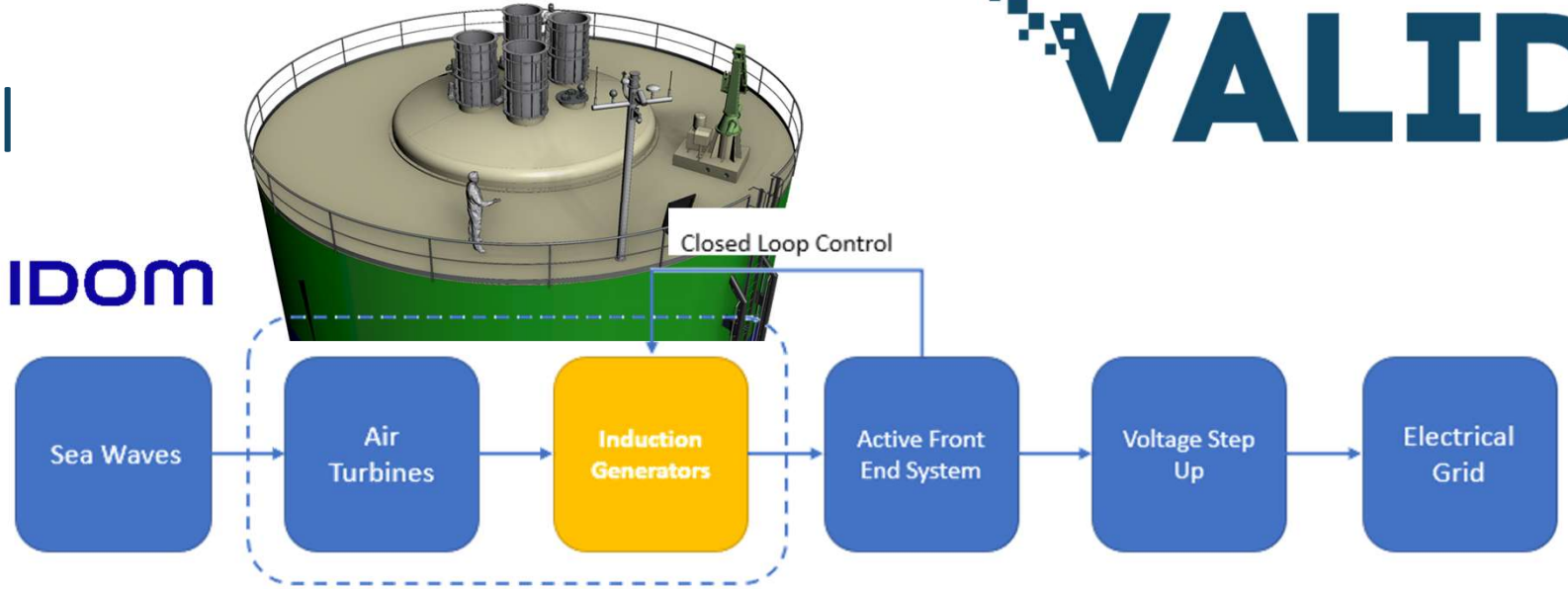


User Case II



The **electrical generator** is in the critical path of the Energy Conversion

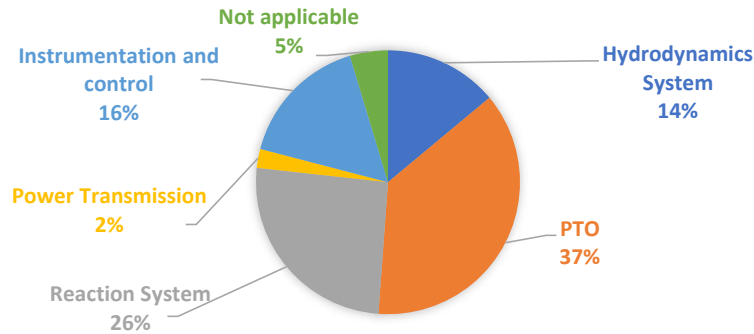
IDOM



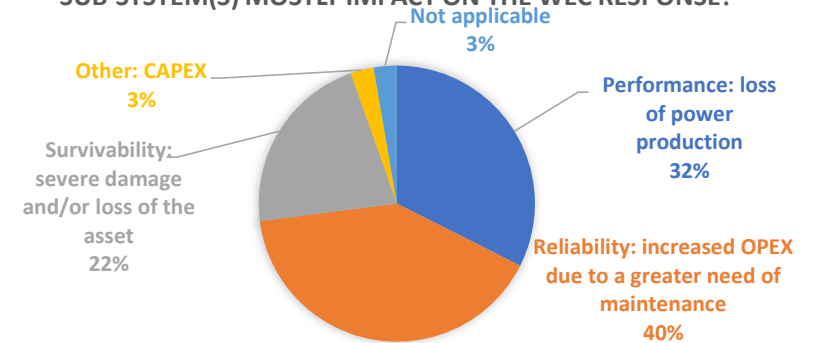
MARMOK PTO



IN YOUR OPINION/EXPERIENCE, WHICH OF THE MAIN SUB-SYSTEMS/COMPONENTS OF THE WEC IS THE MOST CRITICAL?

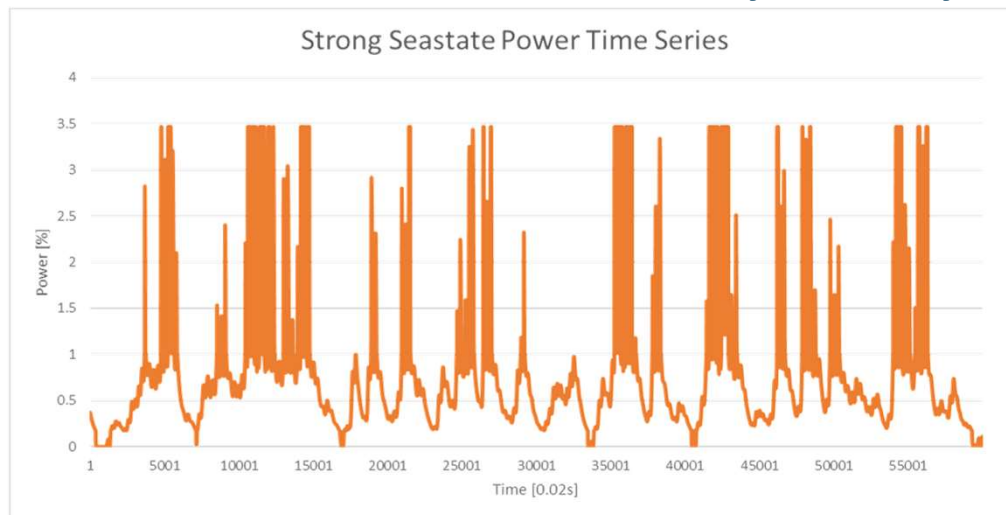


IN YOUR OPINION/EXPERIENCE, WHAT DOES THE CRITICAL SUB-SYSTEM(S) MOSTLY IMPACT ON THE WEC RESPONSE?



Generator Failure

- **Stator winding** accounts for 65% of all failures.
- Stress factors:
 - Thermal degradation – **Temperature**
 - Electrical degradation – **Voltage**
 - External environment – **Humidity & salinity** → difficult to reproduce in the lab

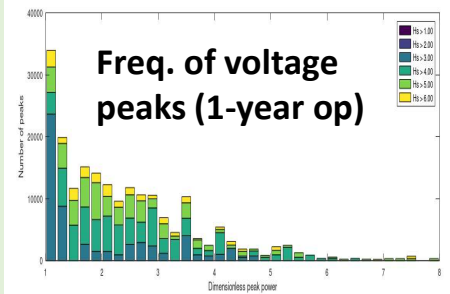
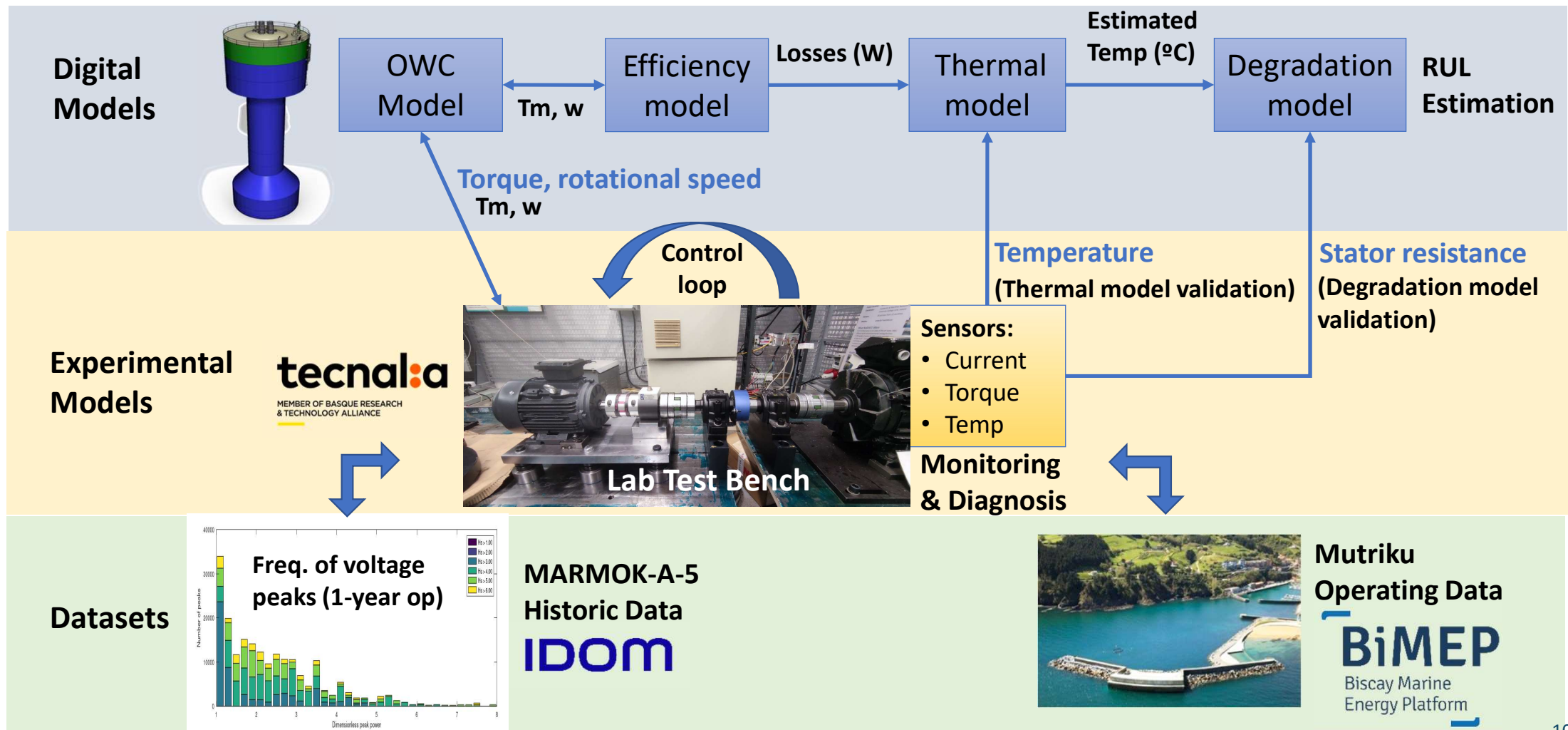


Generator Sizing

Generator	Performance	Survivability	Reliability
Sea State	Ave. to Rated Power	Peak to Rated Power	Overload Time
Mild	17%	1	> 1%
Medium	44%	3.5	6%
Strong	82%	3.5	15%

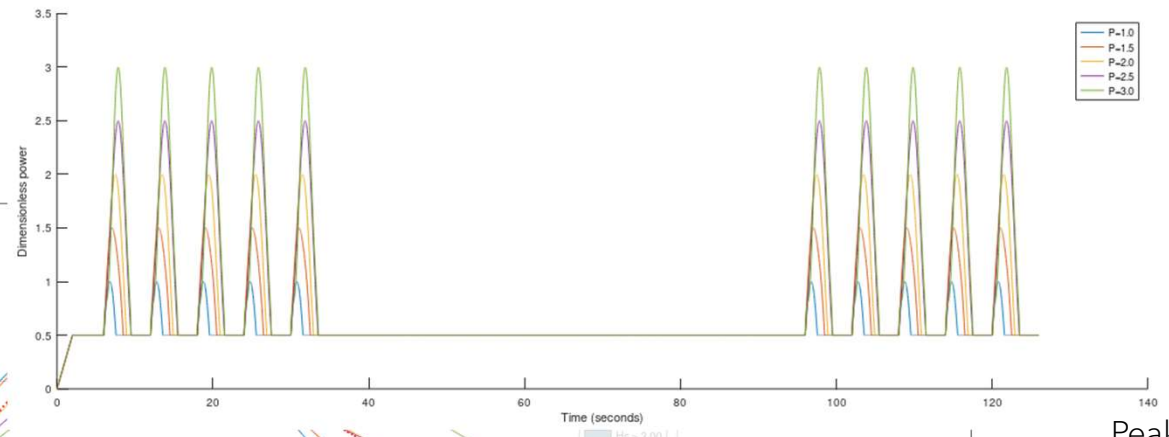


Hybrid Testing Set-Up

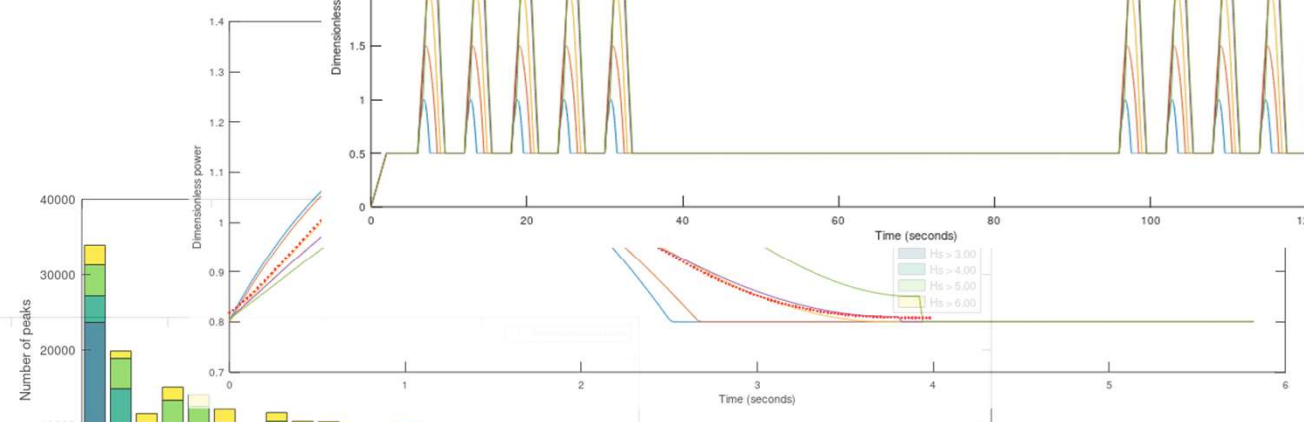


Preprocessing

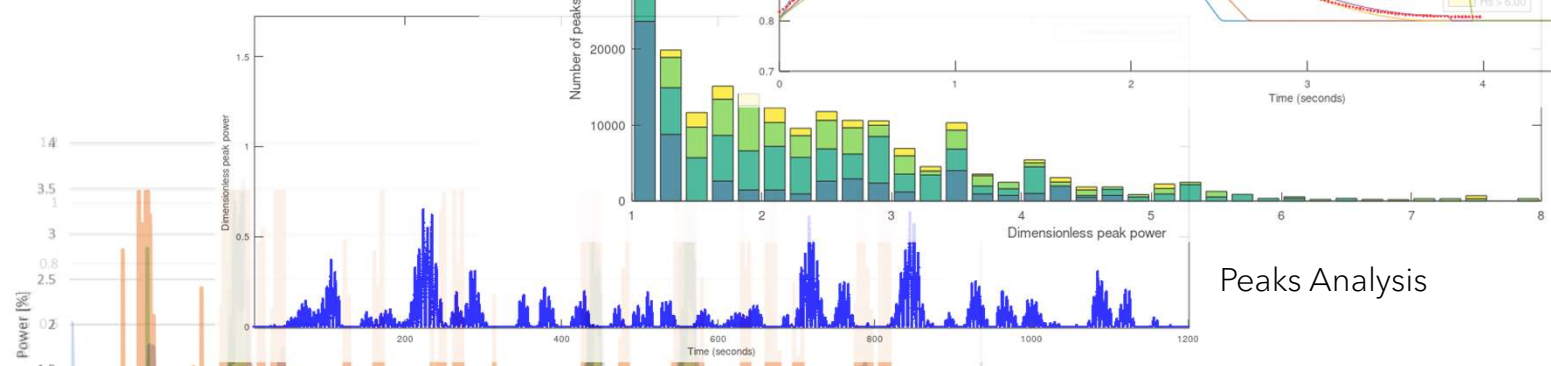
Test Data



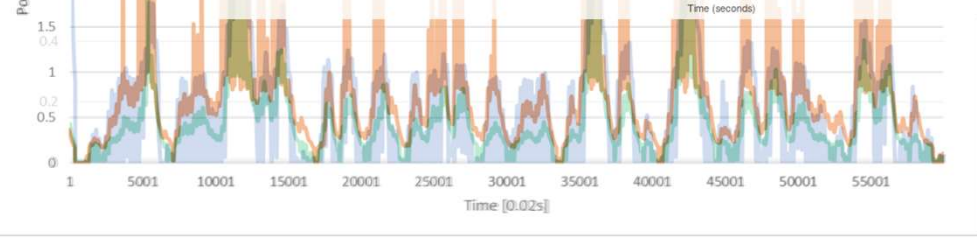
Peak Characterization



Statistic Analysis

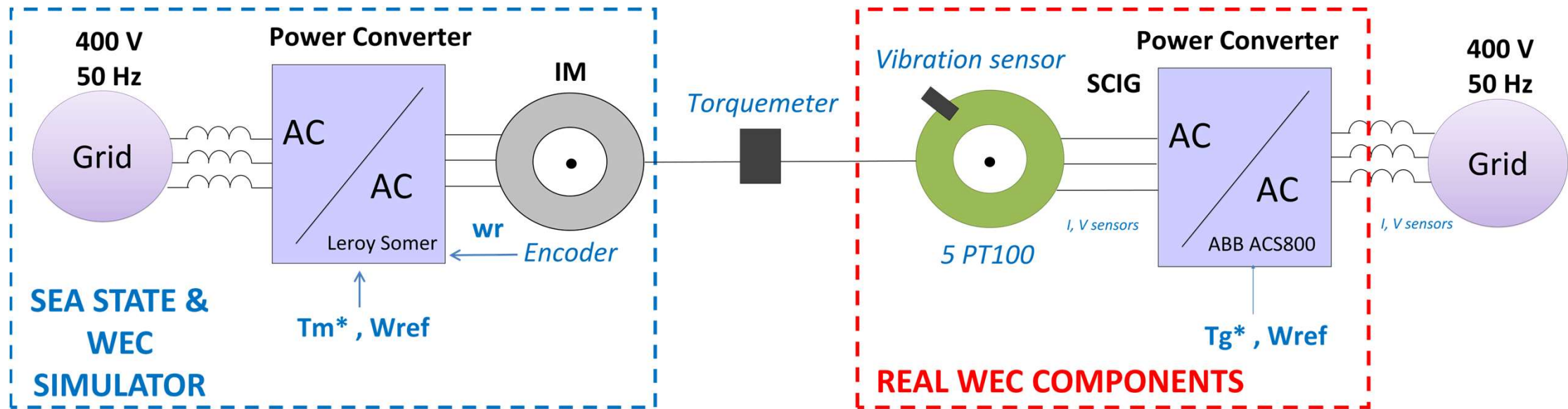


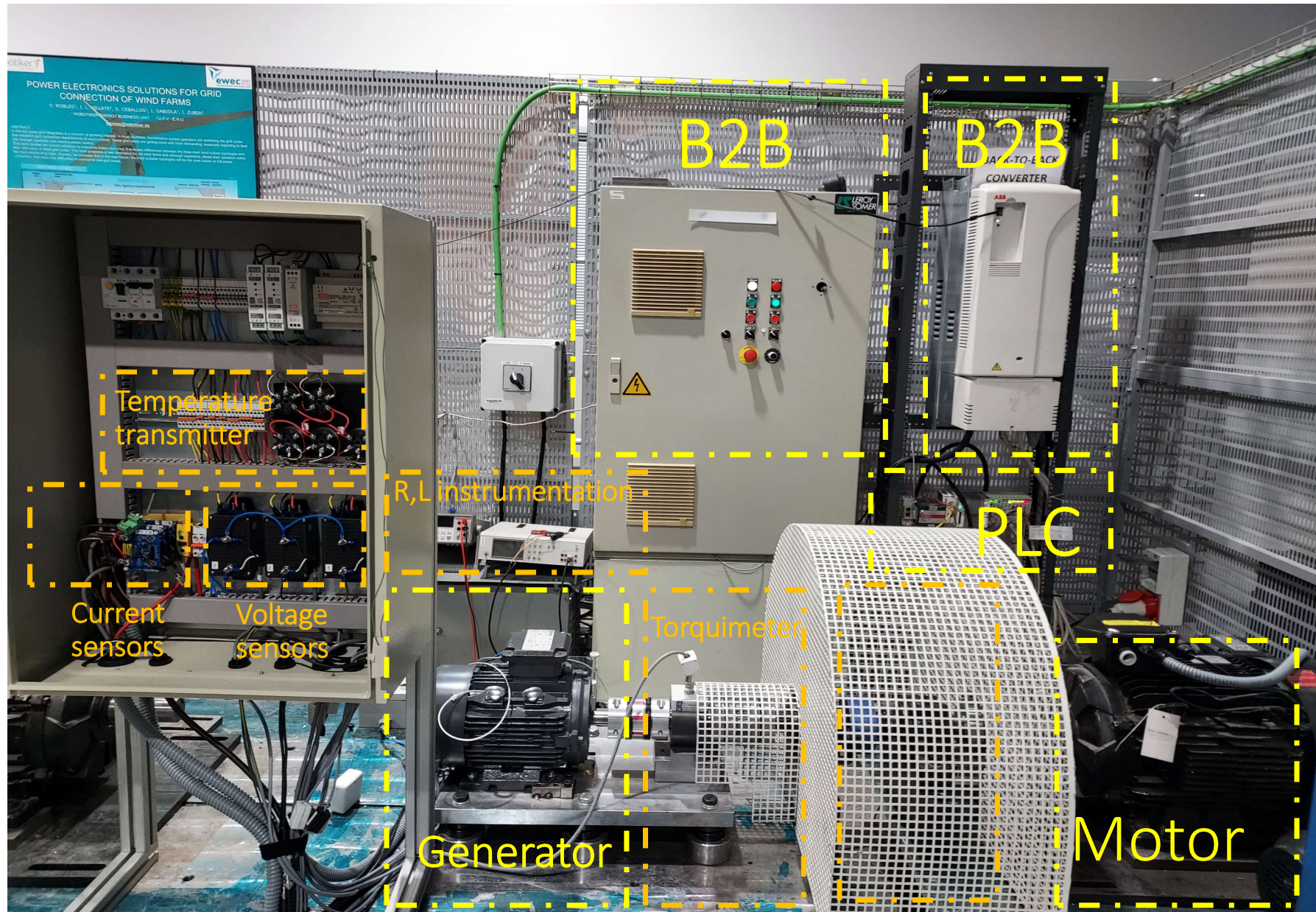
Peaks Analysis



Raw Data Time Series

Test Bench description





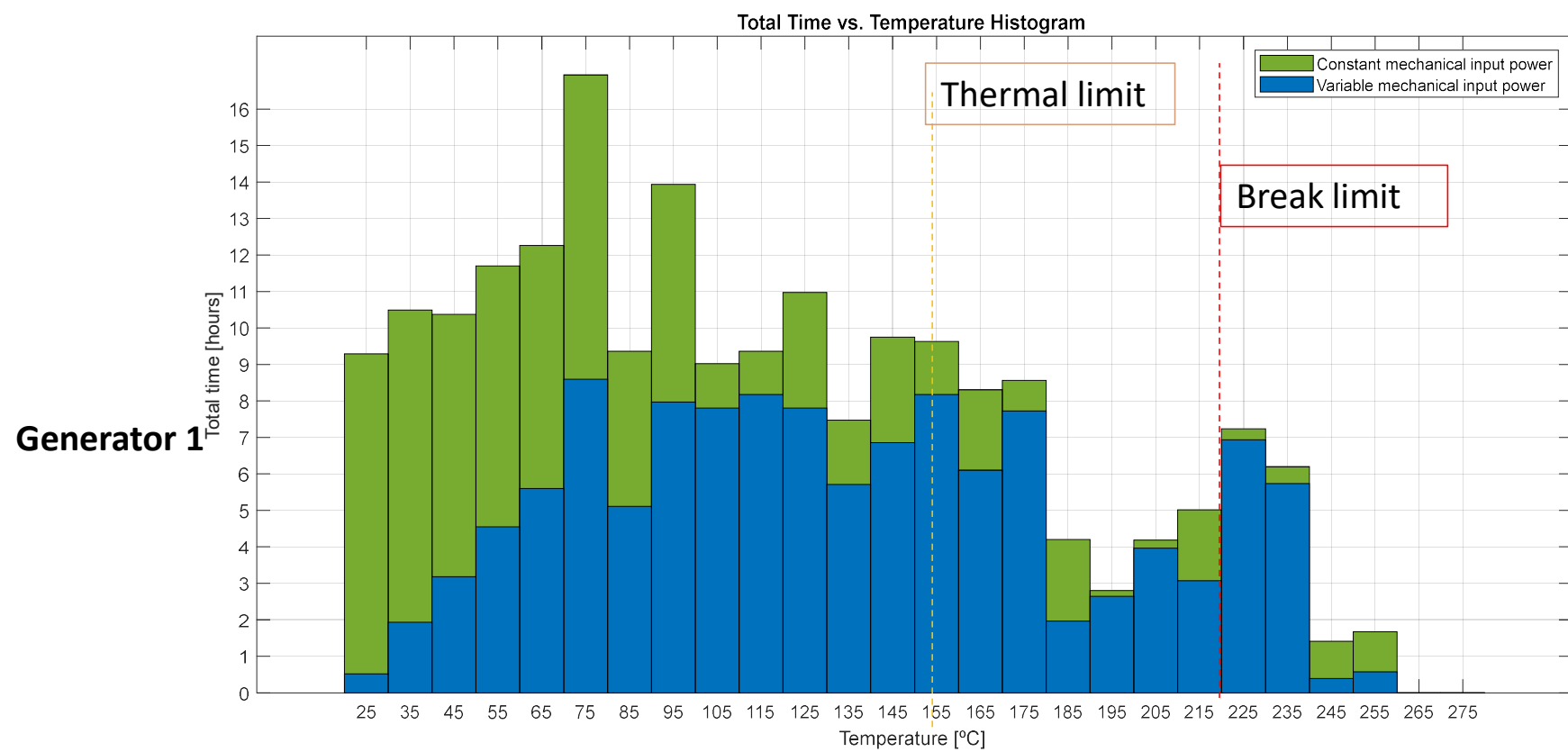
Generator 1: variable working conditions

Test	RMS	Medium	High Peak	Low Peak	Amplitude	Class	Nº of tests
1_Peaks	0,5203	0,4375	0,9974	0,25	0,7474	low	1
2_Peaks	0,7663	0,6085	1,4969	0,25	1,2469	medium	0
3_Peaks	1,0434	1,0129	1,449	0,8	0,649	low	2
4_Peaks	1,1443	1,0265	1,9471	0,6	1,3471	medium	3
5_Peaks	1,2994	1,0201	2,4801	0,3	2,1801	high	1
6_Peaks	0,83	0,8	1,1	0,6	0,5	low	1
7_Peaks	0,9	0,82	1,5	0,5	1	medium	1
8_Peaks	1,04	0,8	2	0,25	1,75	high	1
9_Peaks	1,21	1,19	1,5	1	0,5	low	3
10_Peaks	1,25	1,19	1,9	0,9	1	medium	2
11_Peaks	1,37	1,2	2,35	0,6	1,75	high	2
12_Peaks	1,33	1,32	1,65	1,15	0,5	low	4
13_Peaks	1,37	1,32	2,05	1,05	1	medium	2
14_Peaks	1,45	1,31	2,5	0,75	1,75	high	3
15_Peaks	1,42	1,41	1,8	1,3	0,5	low	1
16_Peaks	1,45	1,4	2,1	1,1	1	medium	1
17_Peaks	1,56	1,42	2,6	0,85	1,75	high	2
18_Peaks	1,53	1,52	1,9	1,4	0,5	low	2
19_Peaks	1,55	1,51	2,2	1,2	1	medium	1
20_Peaks	1,65	1,52	2,7	0,95	1,75	high	3
21_Peaks	1,96	1,64	3,6	0,6	3	extreme	2
22_Peaks	1,61	1,6	1,96	1,46	0,5	low	1
23_Peaks	1,63	1,59	2,3	1,3	1	medium	1
24_Peaks	1,74	1,62	2,8	1,05	1,75	high	1
25_Peaks	1,81	1,8	2,15	1,65	0,5	low	1
26_Peaks	1,84	1,8	2,5	1,5	1	medium	6
27_Peaks	1,92	1,81	3	1,25	1,75	high	1

VALID



Thermal fatigue testing of electric generator

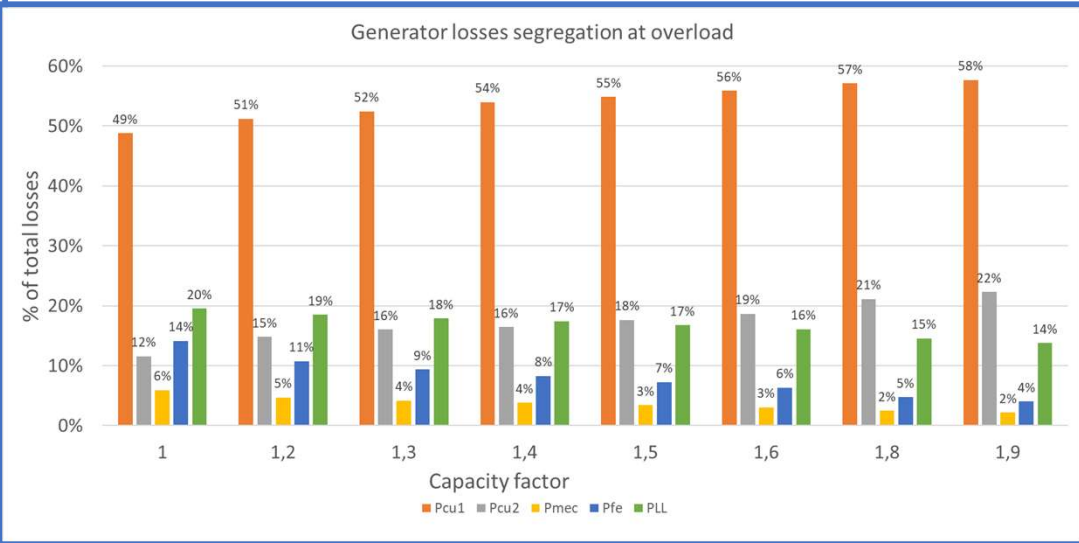
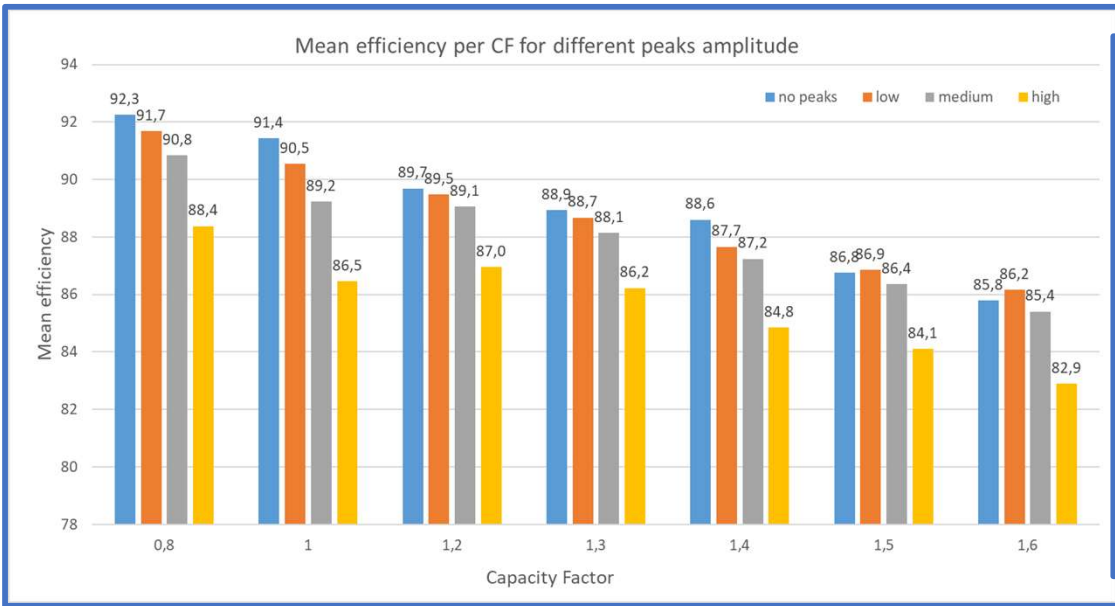
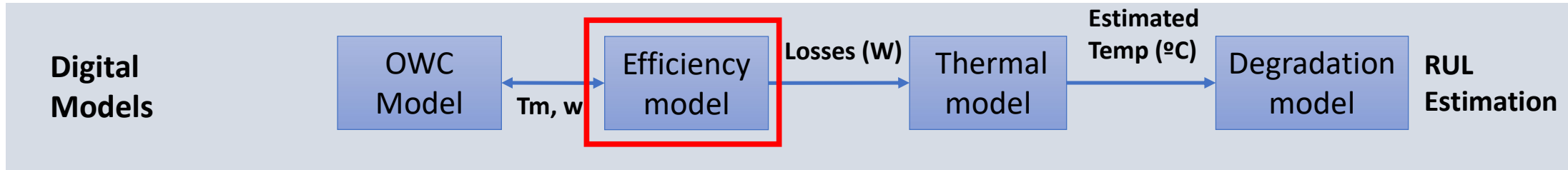


Test plan Generator 2 → no time, harder tests

Test	P rms	P media	P peak	P low	Amplitude	Period
32_Peaks	1,328	1,2	2,25	0,75	1,5	2
33_Peaks	1,414	1,3	2,36	0,86	1,5	2
34_Peaks	1,511	1,4	2,46	0,96	1,5	2
35_Peaks	1,612	1,5	2,54	1,04	1,5	2
36_Peaks	1,692	1,6	2,62	1,12	1,5	2
28_Peaks	1,705	1,7	2,05	1,55	0,5	2
29_Peaks	1,735	1,7	2,4	1,4	1	2
30_Peaks	1,792	1,7	2,72	1,22	1,5	2
31_Peaks	1,819	1,7	2,9	1,15	1,75	2

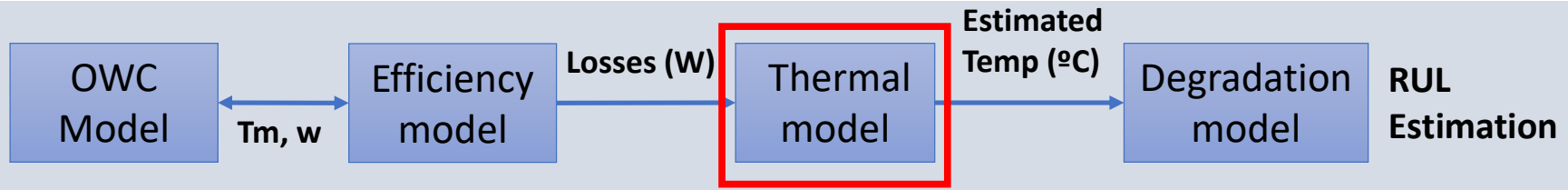


Models, validation and result analysis



*Capacity Factor CF = Torque CF * Speed CF*

Digital Models



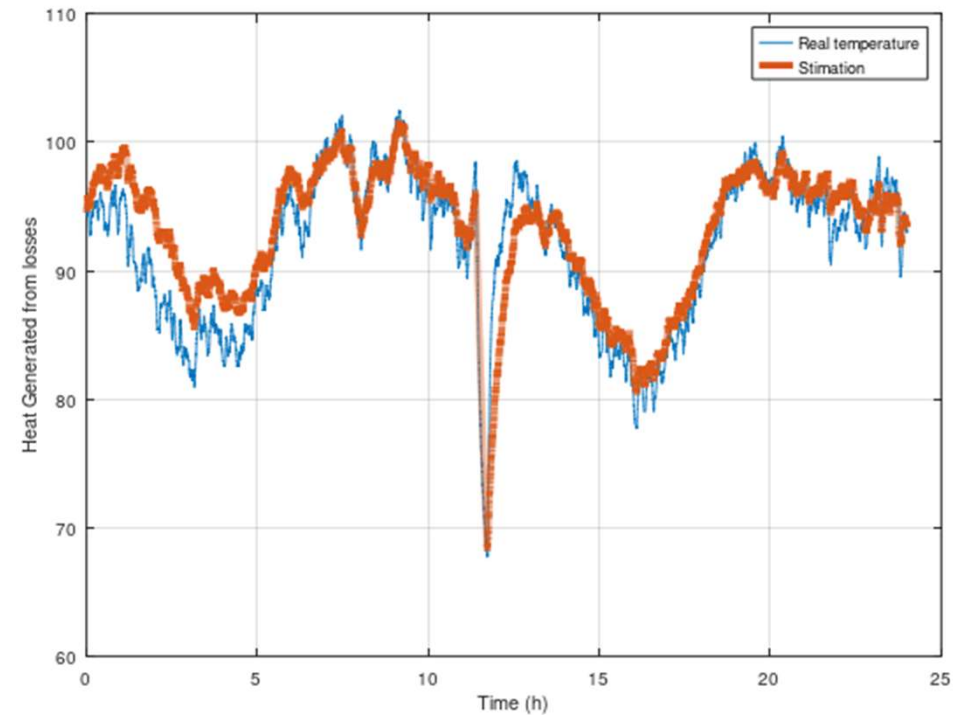
1st Order Thermal Model

$$\theta_{max} = \theta_{SF=1} * \left(\frac{I}{I_{nom}} \right)^2$$

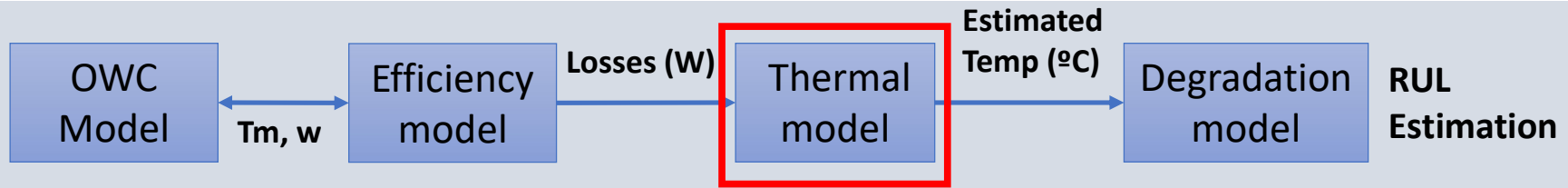
$$\theta = \theta_{max} * \left(1 - e^{-\frac{t}{\tau}} \right) + \theta^{-1} * e^{-\frac{t}{\tau}} + \theta_{amb}$$

Where:

- θ – Actual winding temperature.
- θ_{amb} – Ambient temperature.
- τ_{max} – Maximum temperature increased due to actual stator current.
- θ^{-1} – Previous temperature increase.
- t – Sample time in seconds.
- τ – Heating time constant



Digital Models



2nd Order Thermal Model

$$\theta_{max\ case} = \theta_{SF=1\ case} * \left(\frac{I}{I_{nom}}\right)^2$$

$$\theta_{max\ copper} = \theta_{SF=1\ copper} * \left(\frac{I}{I_{nom}}\right)^2$$

$$\theta_{case} = \theta_{max\ case} * \left(1 - e^{\frac{-t}{\tau_{case}}}\right) + \theta_{case}^{-1} * e^{\frac{-t}{\tau_{case}}}$$

$$\theta_{copper} = \theta_{max\ copper} * \left(1 - e^{\frac{-t}{\tau_{copper}}}\right) + \theta_{copper}^{-1} * e^{\frac{-t}{\tau_{copper}}}$$

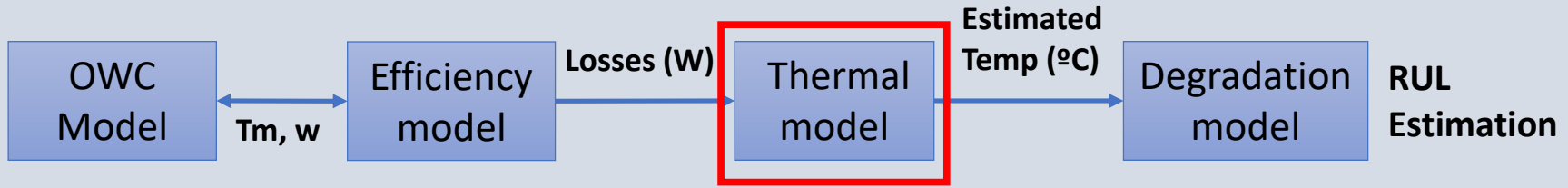
$$\theta = \theta_{copper} + \theta_{case} + \theta_{amb}$$

Where:

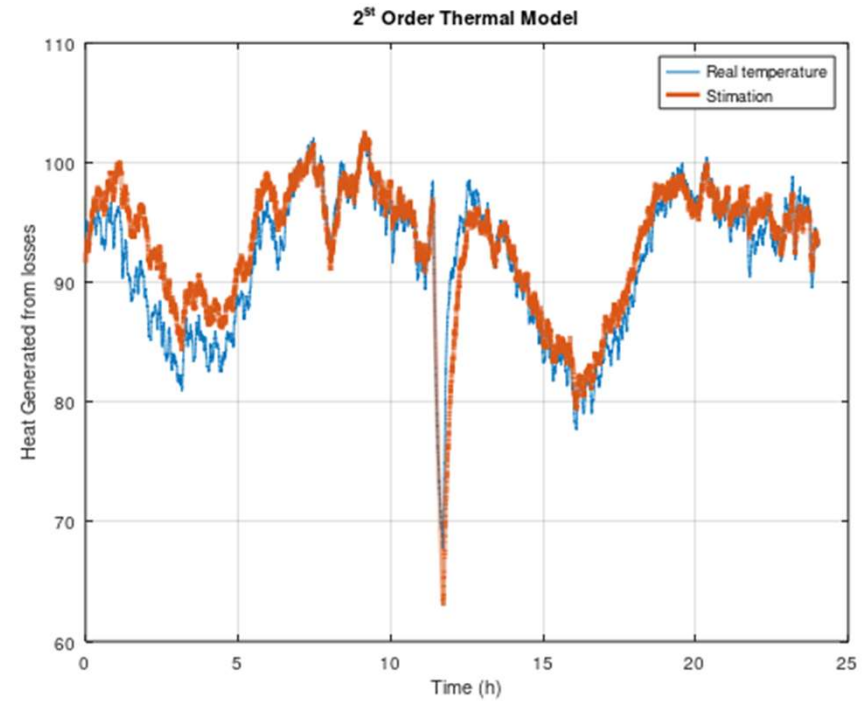
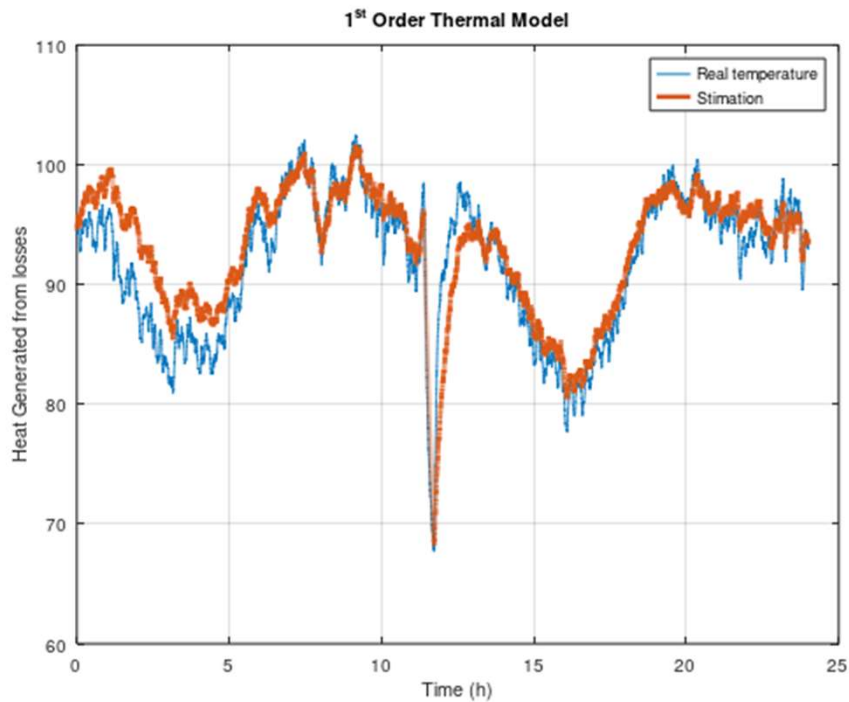
- θ – Actual winding temperature.
- θ_{amb} – Ambient temperature.
- $\theta_{max\ case}$ – Maximum temperature increased due to actual stator current in case.
- $\theta_{max\ copper}$ – Maximum temperature increased due to actual stator current in copper.
- θ_{case}^{-1} – Previous temperature increase in case.
- θ_{copper}^{-1} – Previous temperature increase in copper.
- t – Sample time in seconds.
- τ_{copper} – Heating time constant of copper / steel
- τ_{case} – Heating time constant of case



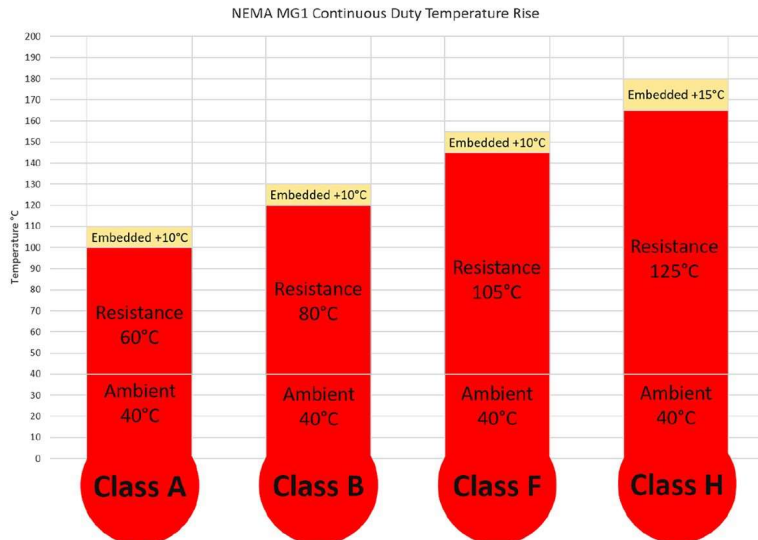
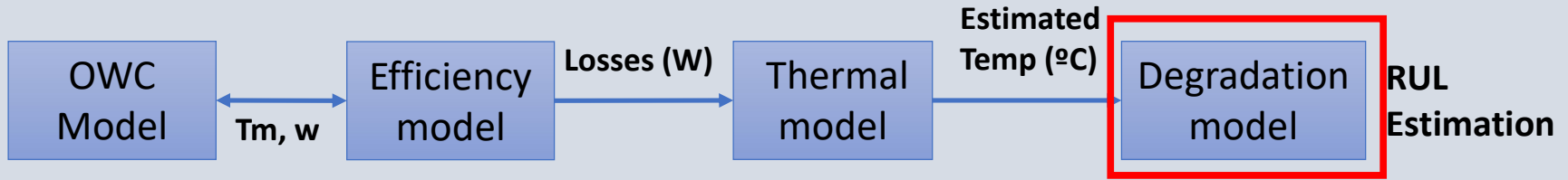
Digital Models



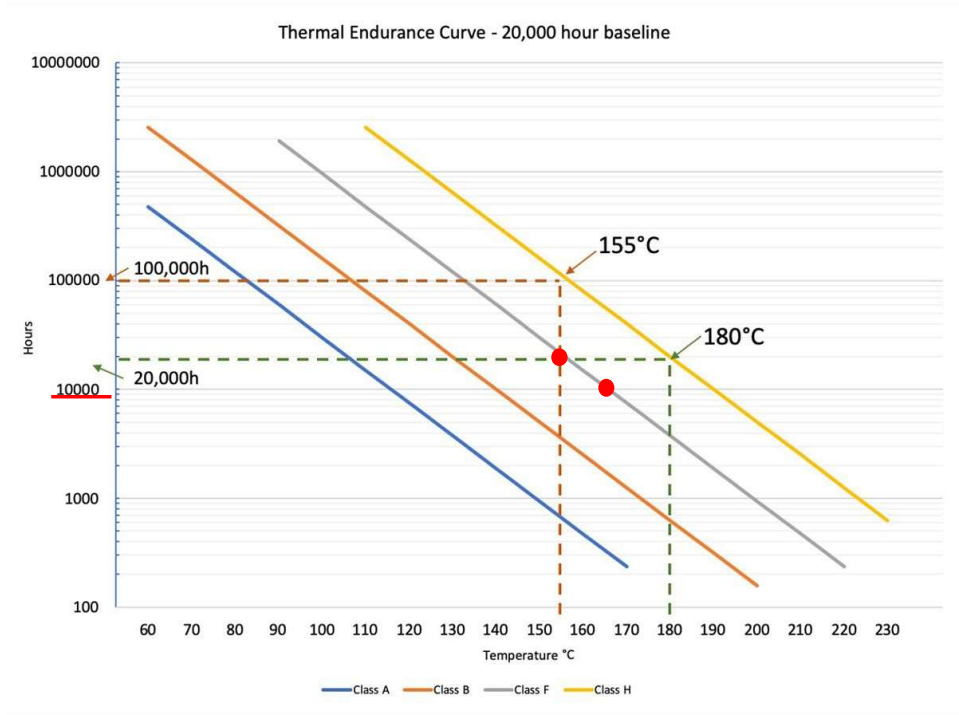
Comparison between models



Digital Models



Arrhenius



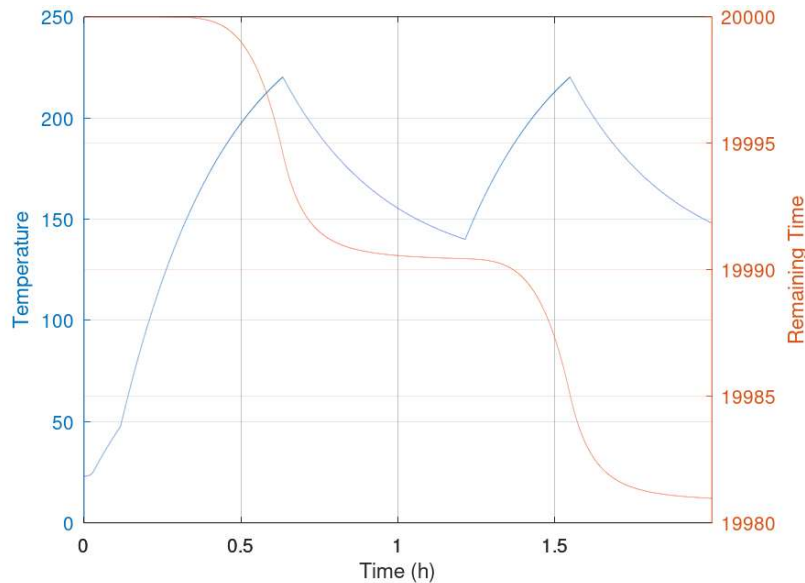
IEC 60034-1





Modified Arrhenius model

$$L = Ae^{B\left(\frac{1}{\theta_i} - \frac{1}{\theta_0}\right)} \longrightarrow \log_e(t) = C_1 + \frac{C_2}{T}$$



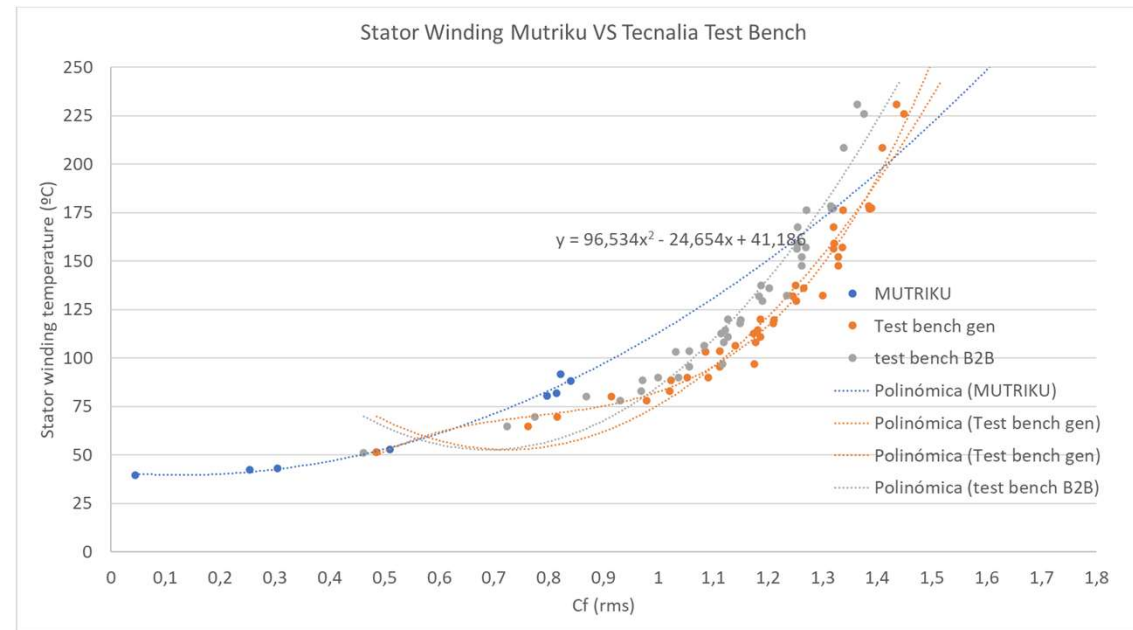
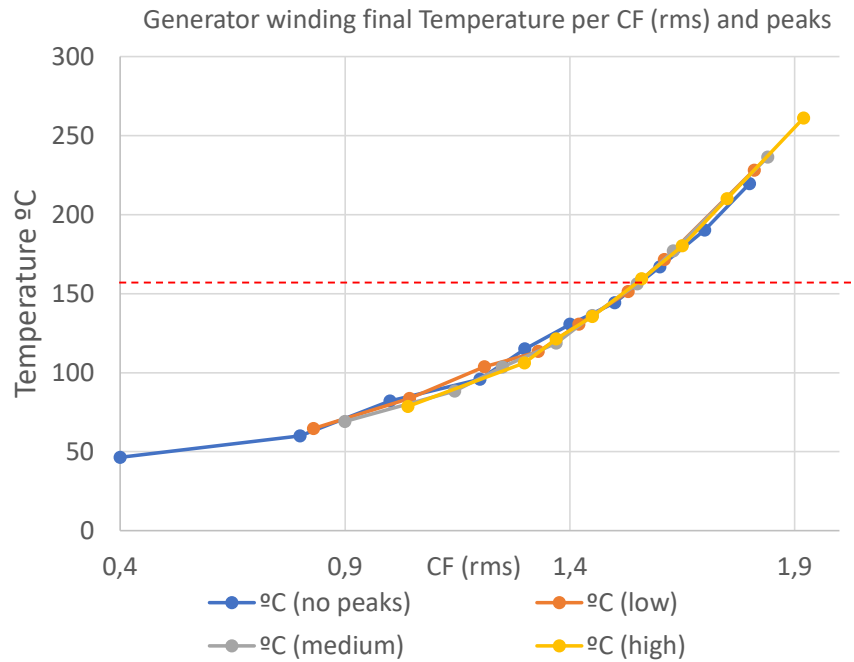
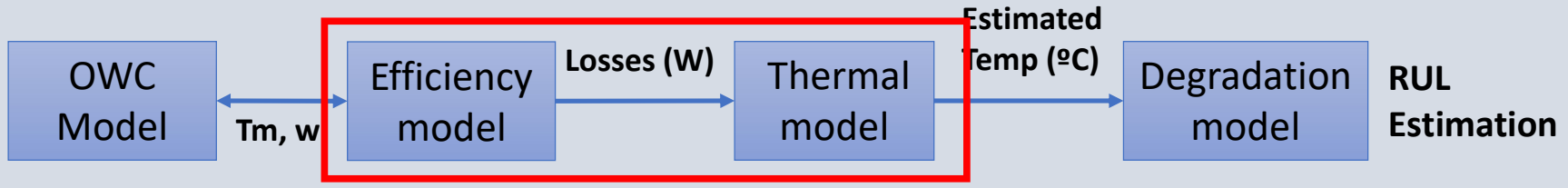
Rule-of-thumb (IEEE Std 117-2015)

Table 1—Temperature and exposure guide (estimated hot-spot temperature range)

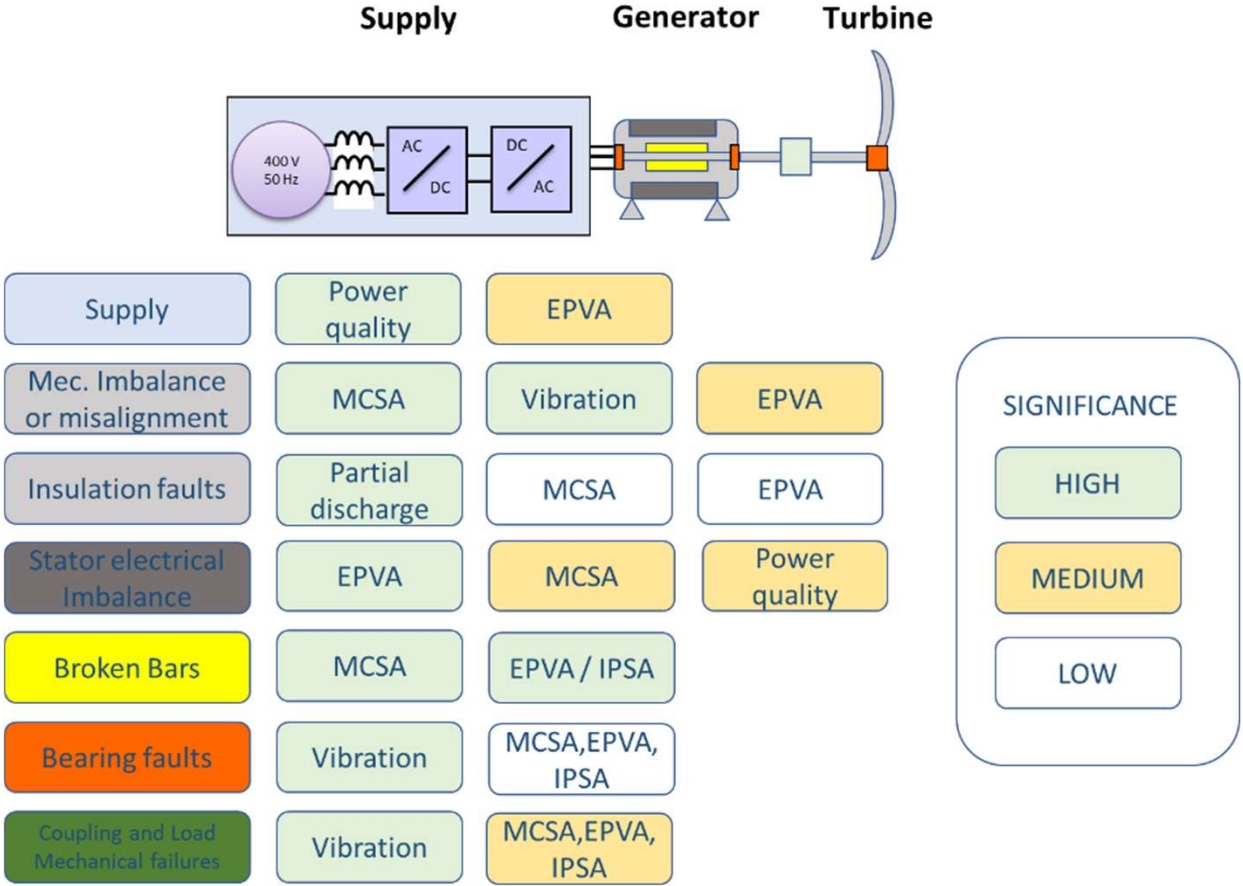
Exposure temperature	Aging (temperature exposure) cycles (in days) for various insulation classifications in °C						
	105 °C (days) (A)	130 °C (days) (B)	155 °C (days) (F)	180 °C (days) (H)	200 °C (days) (N)	220 °C (days) (R)	240 °C (days) (S)
310 °C							1
300 °C							2
290 °C						1	4
280 °C						2	8
270 °C					1	4	16
260 °C					2	8	32
250 °C				1	4	16	
240 °C				2	8	32	
230 °C				4	16		
220 °C			1	8	32		
210 °C			2	16			
200 °C		1	4	32			
190 °C		2	8				
180 °C	1	4	16				
170 °C	2	8	32				
160 °C	4	16					
150 °C	8	32					
140 °C	16						
130 °C	32						



Digital Models



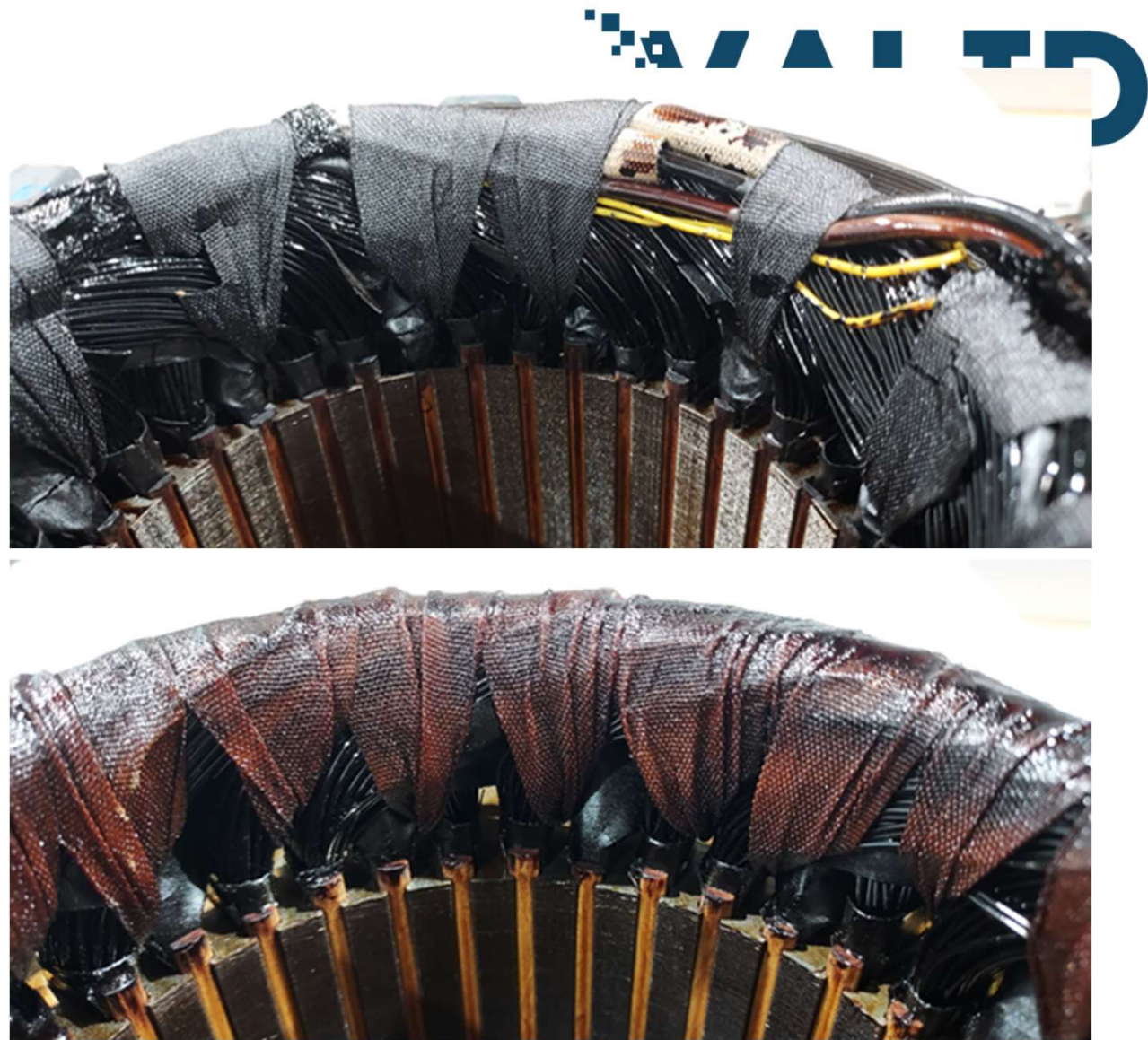
Condition monitoring: Degradation estimation



Failure
detection



burned
stator
winding



Base test(healthy) vs Final test (detected stator winding frequencies)

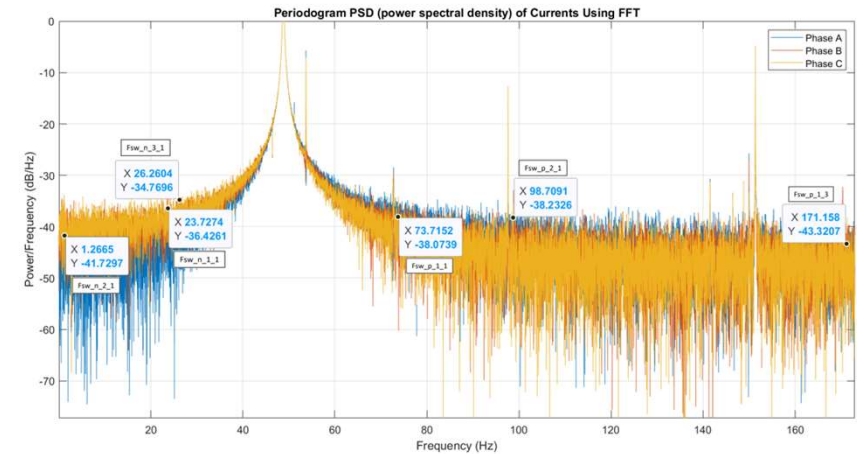
- Identification is made with the following expresión:

$$f_{sw} = f_s \left[k \left(\frac{1-s}{p} \right) \pm n \right]$$

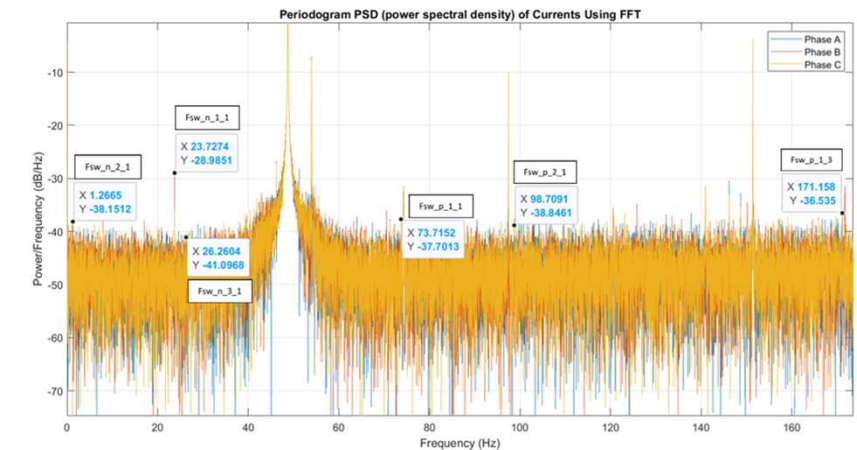
- fsw -> Stator winding failure freq.
- fs -> Supply frequency
- s -> Slip
- p -> pole pair
- k (k=1,2,3...) ->Stator winding constant.
- n (n=1,2,3...) -> Constant

Detected frequency	Final condition
Fsw	1.2665, 23.7274, 26.2604, 73.7152, 98.7091, 171.158

Base test



Final test



Main Challenges

- **Uncertainties:**
 - Correlation between instantaneous power peaks and corresponding sea states
 - Real doubt if these high temperatures will be achieved in the sea
 - Uncertainty in when the generator is going to break
- **Thermal model:**
 - Accurate thermal model for the whole operation range
 - Scalability
- **Condition monitoring:**
 - Difficulties in estimating progressive degradation until real breakage
- **Amount of information:**
 - Information of only 1 generator or maximum 2 generators. Not enough for conclusions



Programme

14:00-14:05 Welcome

Paula Garcia Rosa (IMPACT/SINTEF)

14:05-14:30 VALID session

WEC hybrid testing: Lessons learned from IDOM's case study

Iván Ruibal (IDOM)

Eider Robles Sestafe (Tecnalia)

14:30-14:55 IMPACT session

Experience from designing and executing tests on Carnegie Clean Energy's CETO 6 belt

Giacomo Alessandri (VGA)

Sam Neilson (Carnegie Clean Energy)

14:55-15:25 Panel discussion and Q&A session with the presenters

Moderator: Claudia Sans (VALID/Aquatera)

15:25-15:30 Close

Paula Garcia Rosa (IMPACT/SINTEF)



Joint Webinar
January 2024

